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Nelson et al.

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[54] THERMAL AND CHEMICAL REMEDIATION OF MIXED WASTES

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### Related U.S. Application Data

[63] Continuation-in-part of Ser. No. 55,360, Apr. 29, 1993, Pat. No. 5,335,609.

[51] Int. Cl.<sup>6</sup> ..... F23J 11/00

[52] U.S. Cl. .... 110/345; 110/346; 110/215; 110/204

[58] Field of Search ..... 110/215, 245, 110/345, 346, 204, 246; 422/139

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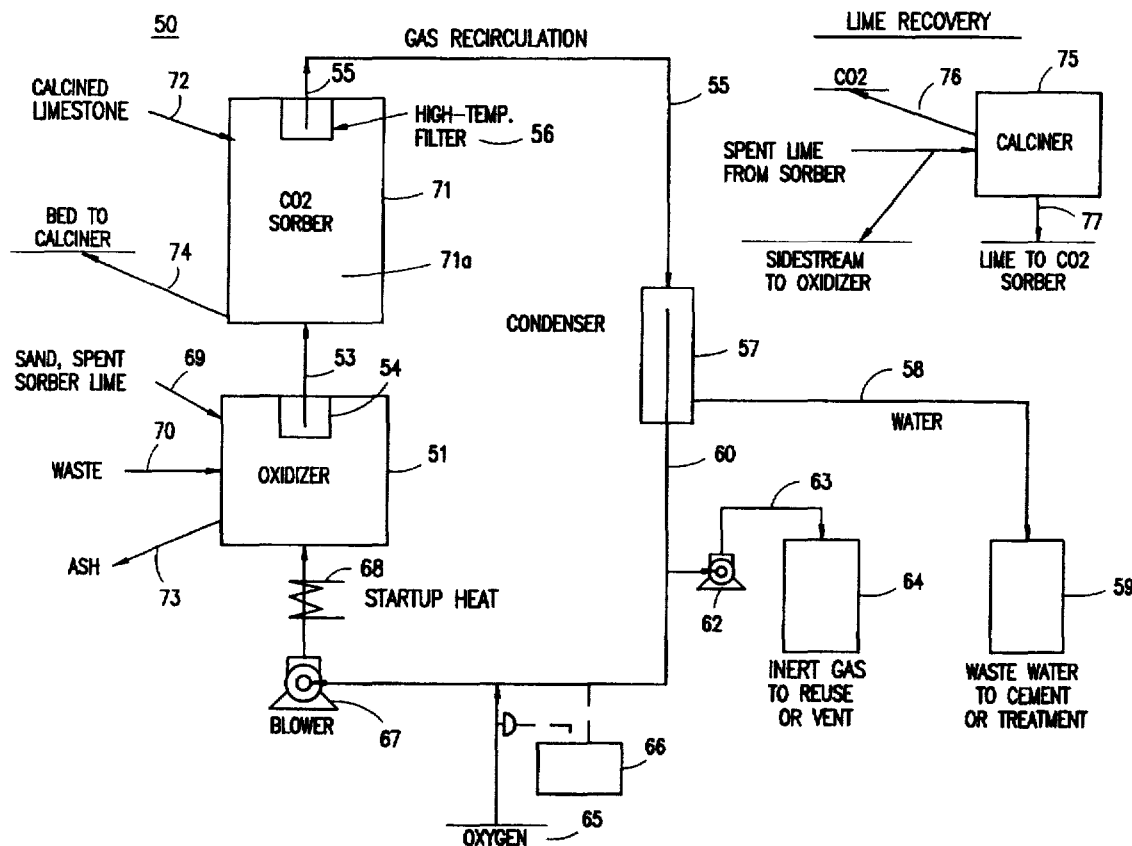
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Attorney, Agent, or Firm—Emrich & Dithmar

### [57] ABSTRACT

A process for treating organic waste materials without venting gaseous emissions to the atmosphere which includes oxidizing the organic waste materials at an elevated temperature not less than about 500° C. with a gas having an oxygen content in the range of from about 20% to about 70% to produce an oxidation product containing CO<sub>2</sub> gas. The gas is then filtered to remove particulates, and then contacted with an aqueous absorbent solution of alkali metal carbonates or alkanolamines to absorb a portion of the CO<sub>2</sub> gas from the particulate-free oxidation product. The CO<sub>2</sub> absorbent is thereafter separated for further processing. A process and system are also disclosed in which the waste materials are contacted with a reactive medium such as lime and product treatment as described.

9 Claims, 8 Drawing Sheets



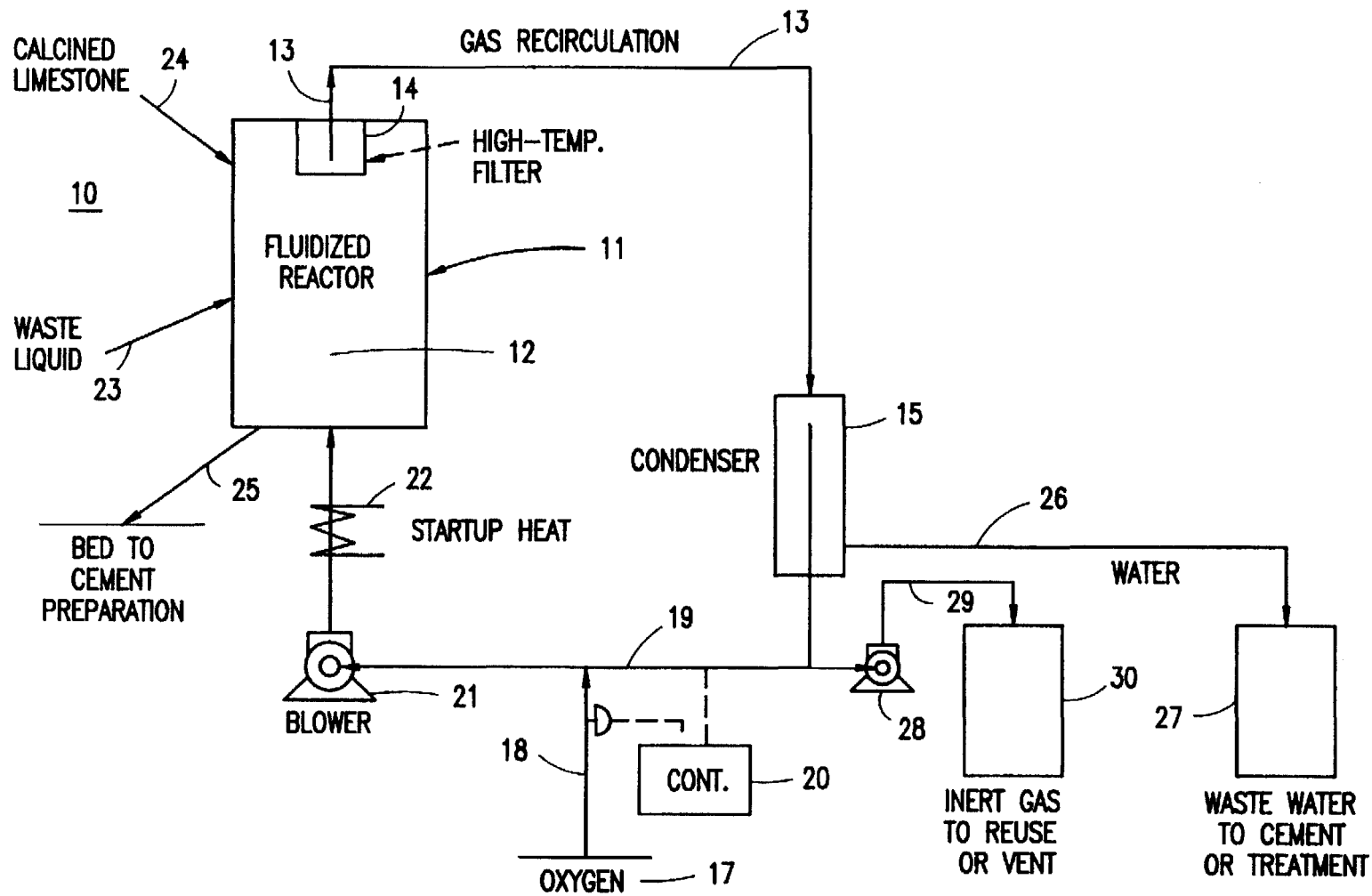


Fig. 1

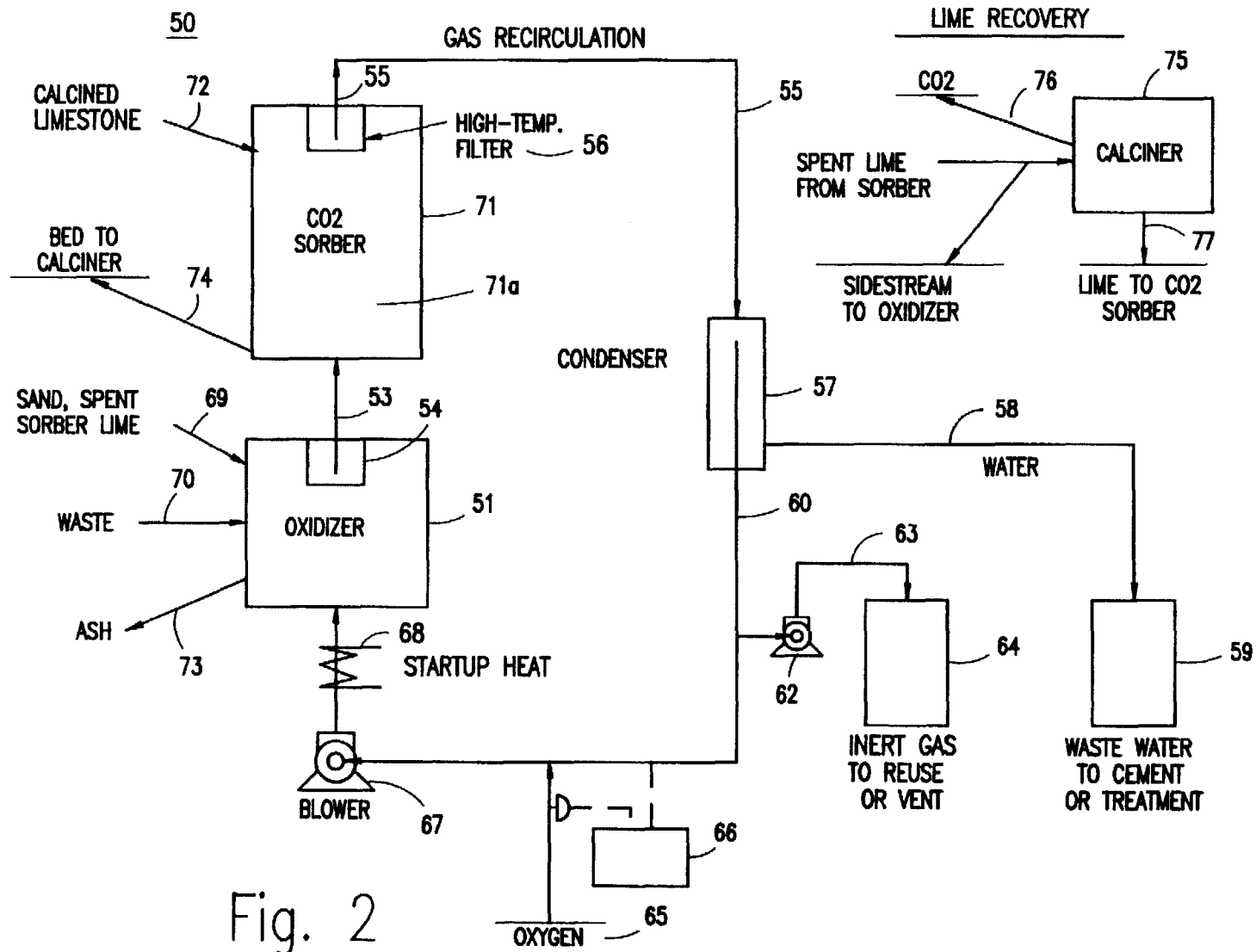


Fig. 2

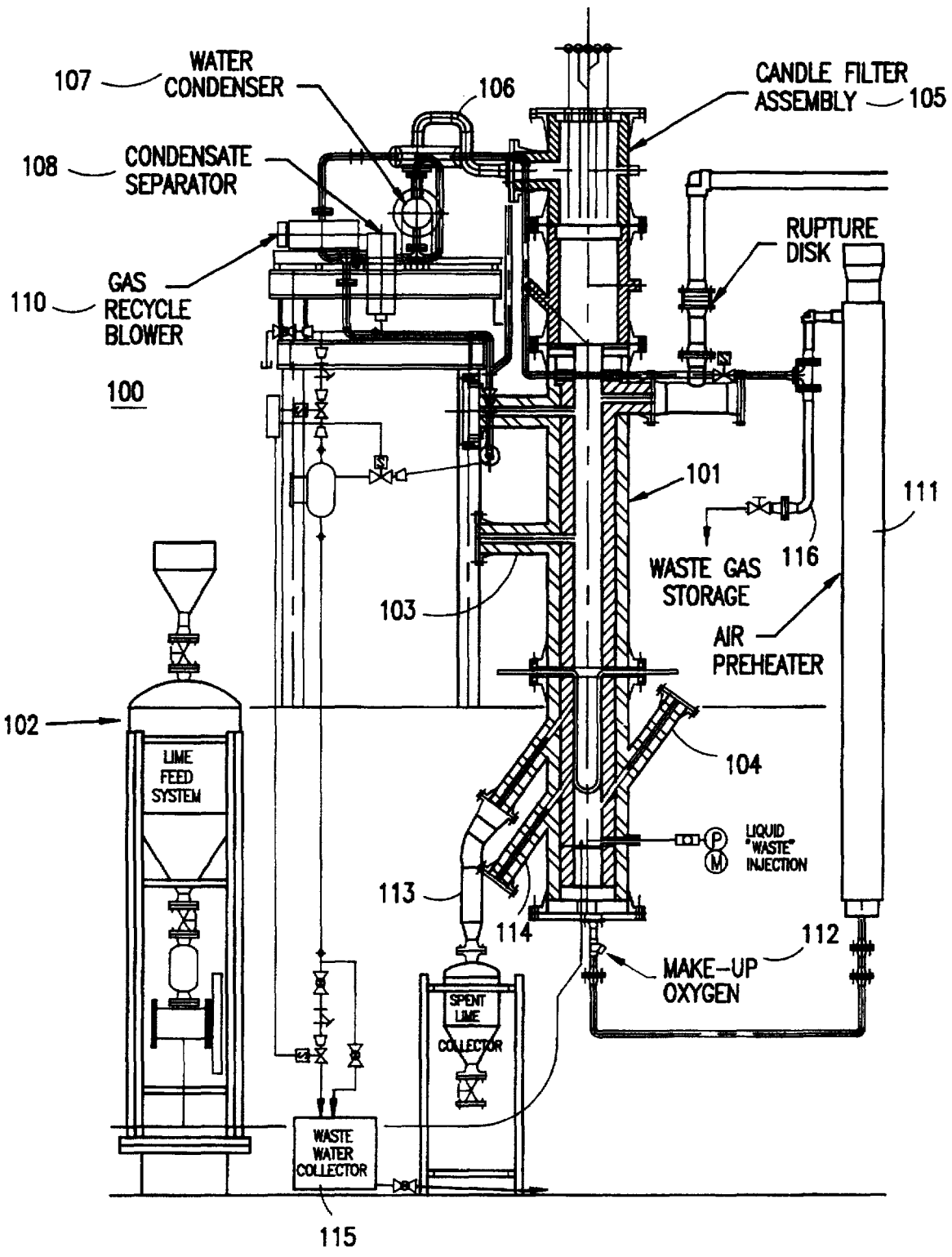


Fig. 3

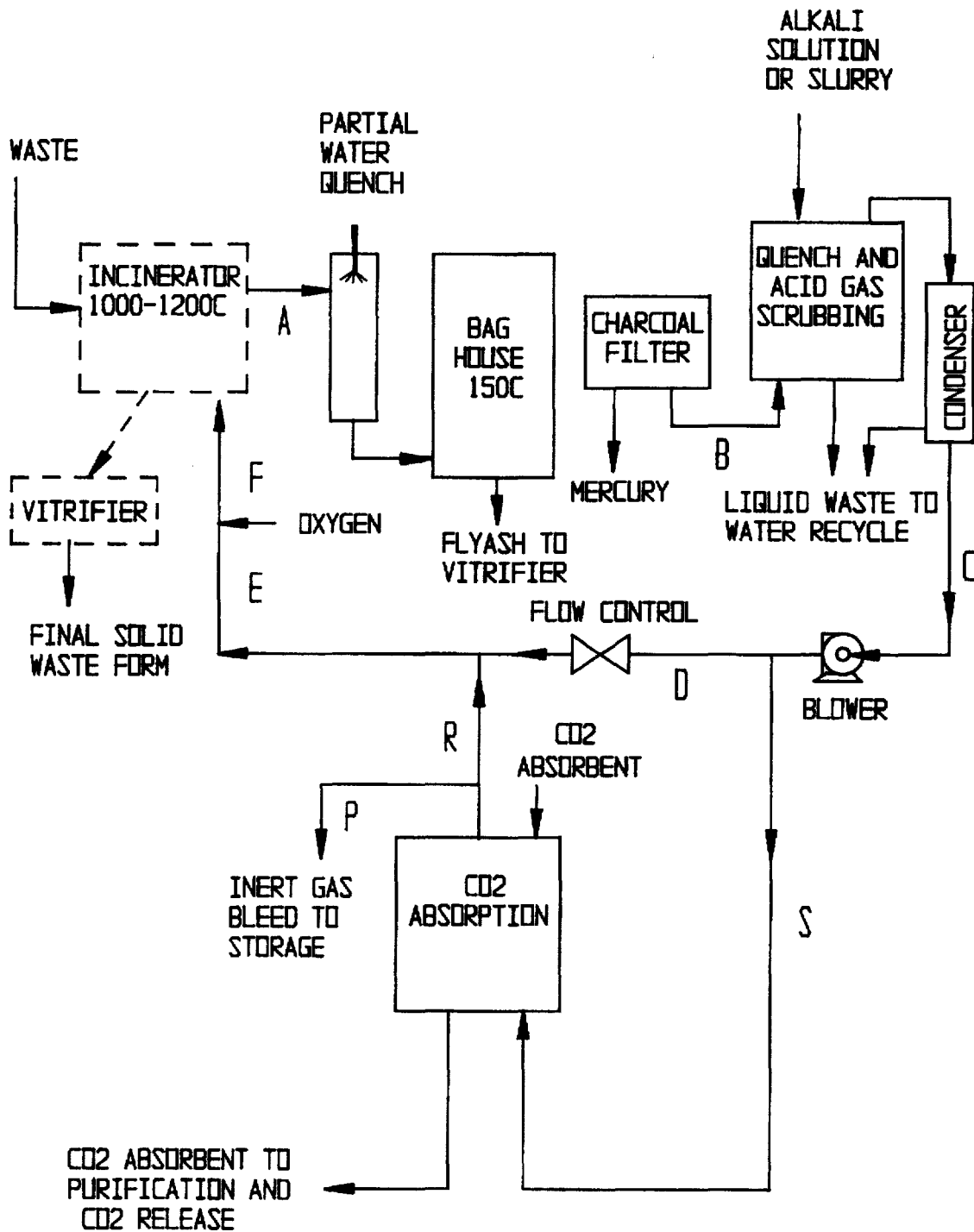


Fig. 4

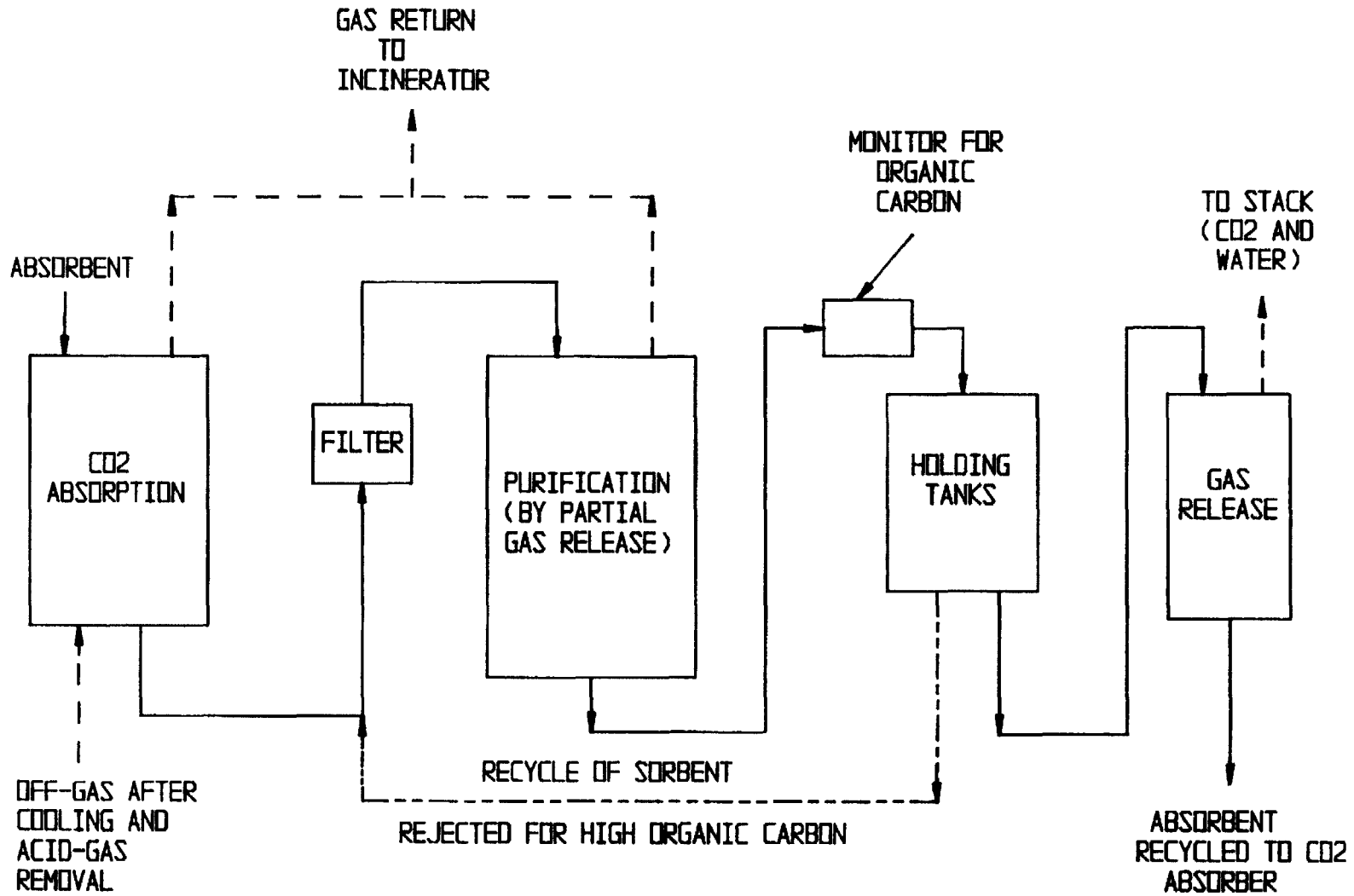


Fig. 5

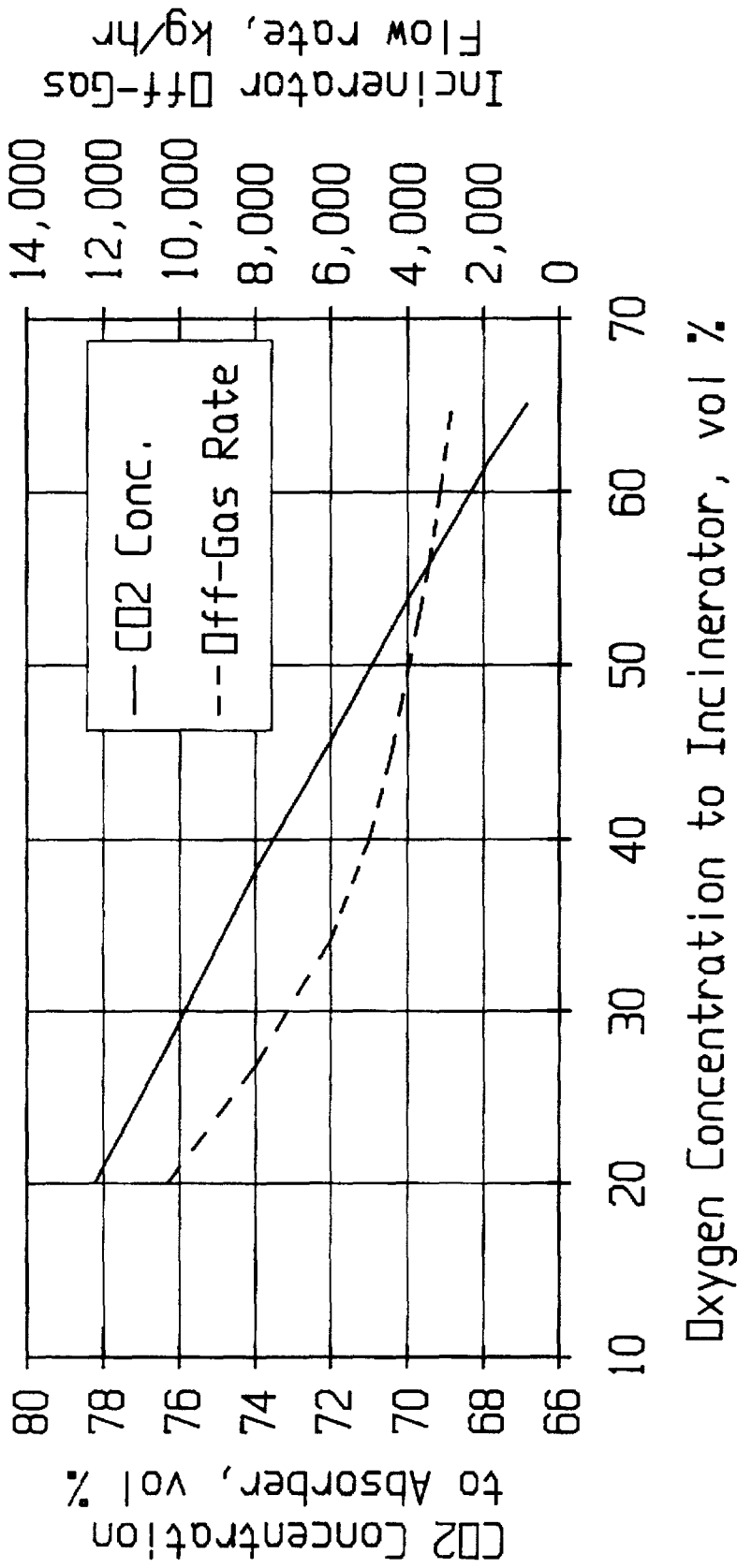


Fig. 6

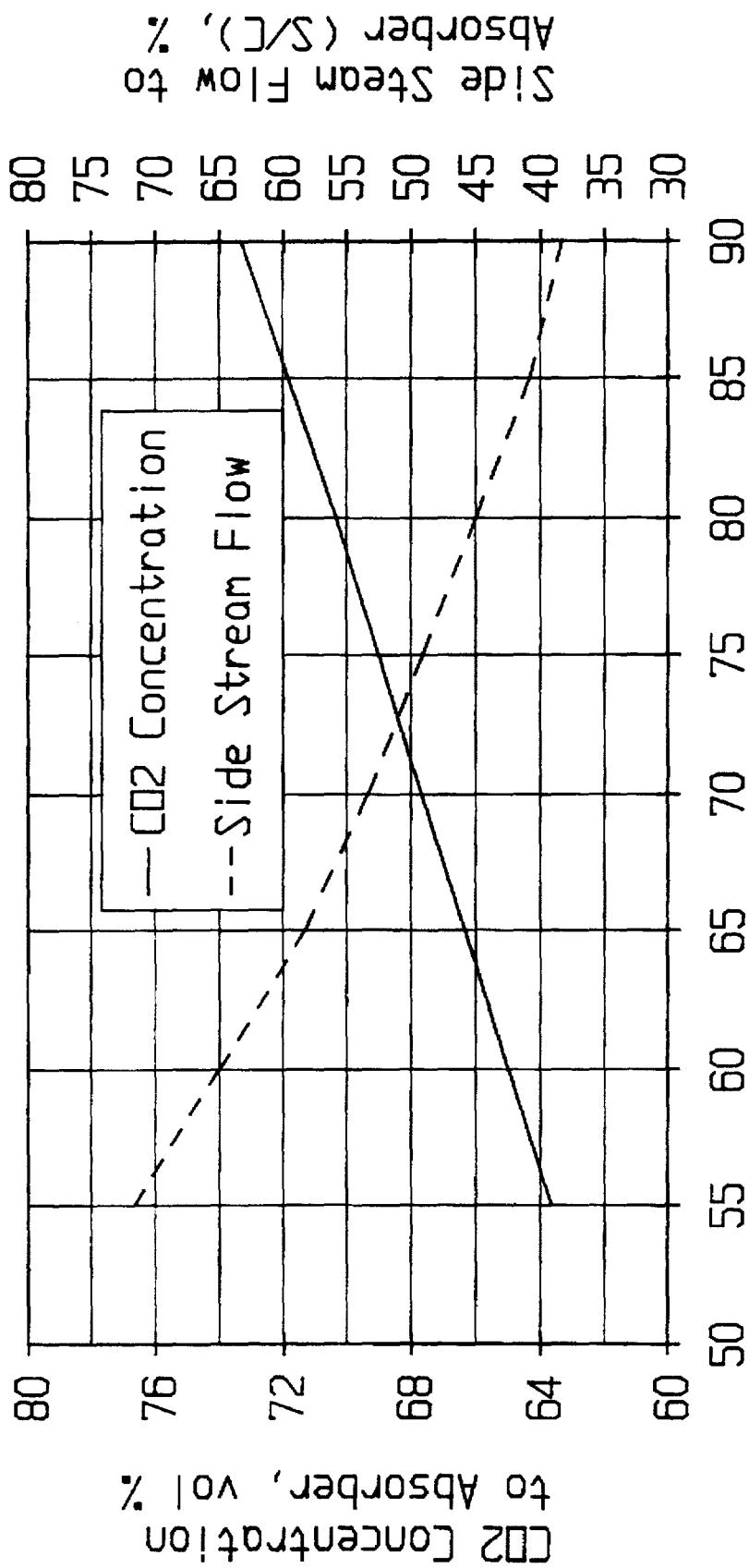


Fig. 7

CO2 Absorption Efficiency



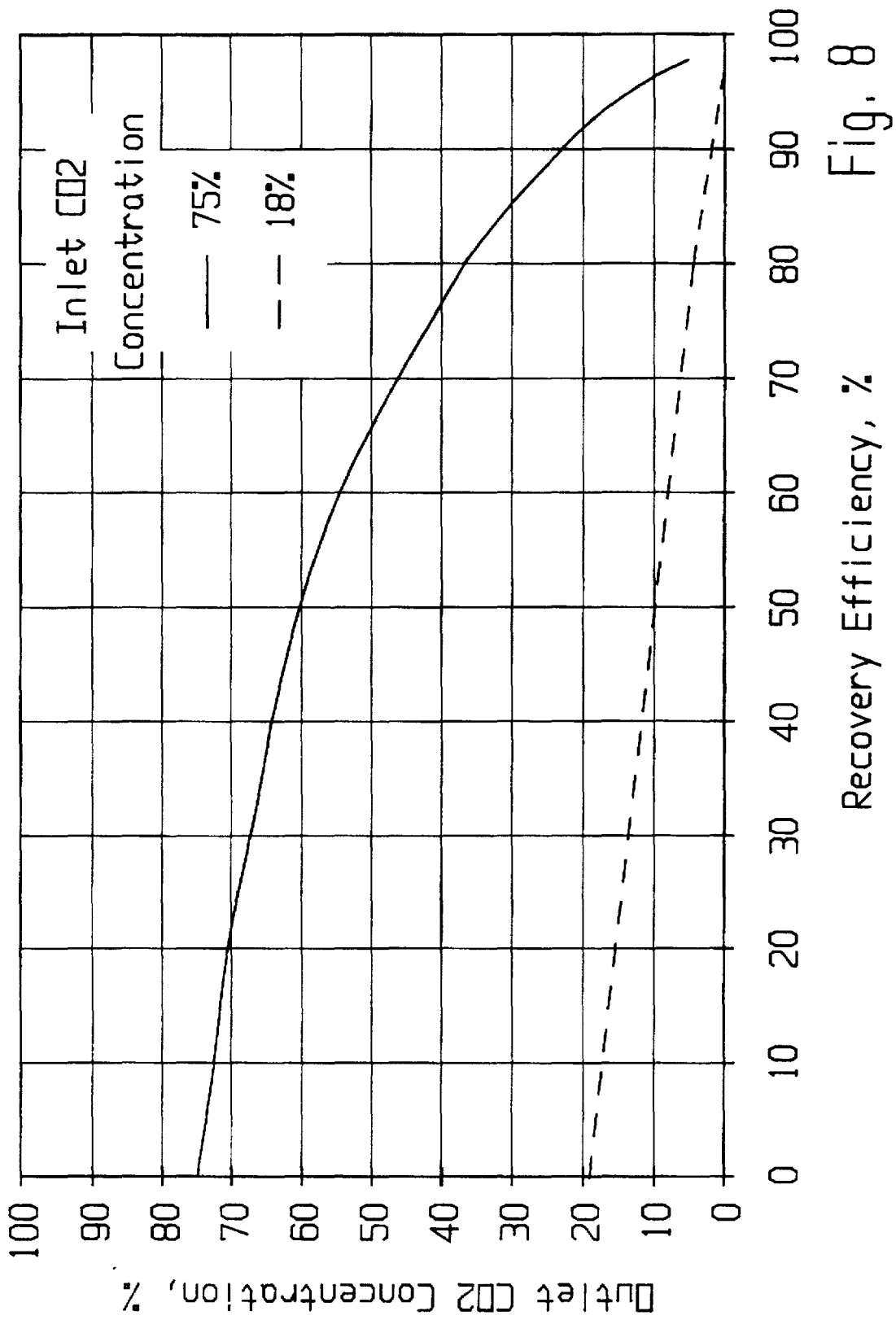


Fig. 8

## THERMAL AND CHEMICAL REMEDIATION OF MIXED WASTES

### RELATED APPLICATION

This is a continuation-in-part application of Ser. No. 08/055,360, filed Apr. 29, 1993, now U.S. Pat. No. 5,355,609.

### CONTRACTUAL ORIGIN OF THE INVENTION

The United States Government has rights in this invention pursuant to Contract No. W-31-109-ENG-38 between the U.S. Department of Energy and The University of Chicago representing Argonne National Laboratory.

### BACKGROUND OF THE INVENTION

When operated properly, incinerators can achieve high efficiency in destroying hazardous organic materials in treating both hazardous wastes and mixed wastes. However, problems arise during improper operations or upset conditions, when dioxanes, furans, and other toxic materials may be released at dangerous levels. By means of careful design and operation, which are regulated by the Environmental Protection Agency, and various state and local agencies, dangerous emission levels can be avoided.

Fluid bed incineration for hazardous organic waste is an old concept and has been practiced for years by several companies, one of which being the Dorr-Oliver Company. In the June, 1992 edition of "Chemical Engineering Progress", John F. Mullin of the Dorr-Oliver Company reviewed the waste incinerator designs used to treat hazardous waste over the past fifteen years. Examples of the Dorr-Oliver technology are included in the Fitch et al. U.S. Pat. No. 4,159,682 issued Jul. 3, 1979 showing separate dryer and incinerator fluid beds wherein the dryer off gases are handled separately from the incinerator off gases and hot bed material from the incinerator is used to heat the moist feed material to the dryer. However, the Fitch et al. '682 patent vents incinerator off gases to the atmosphere. Another Dorr-Oliver patent is the Fitch et al. U.S. Pat. No. 4,232,614 issued Nov. 11, 1980, which also teaches separate air dryer and incinerator mechanisms, both of which have off gas streams which are treated separately but which eventually exit the system to the atmosphere.

Another company that has been active in the incineration of hazardous waste material was the Envirotech Corporation of Menlo Park, Calif., later bought by the Lurgi Company. However, in the 70's and early 80's, the Envirotech Company operated a number of systems in an attempt to treat sewage sludge and industrial waste. Representative systems include rotary kiln systems and multiple hearth systems which were used to classify and dry sludge and thereafter incinerate same, for instance see the Isheim U.S. Pat. No. 4,153,411, the Isheim U.S. Pat. No. 4,248,164, the Lombana U.S. Pat. No. 4,215,637. There are other patents issued to Envirotech which are also pertinent; however, none of these patents relate to systems in which no vapor emissions exit to the atmosphere.

Briefly, other companies through the years, have used fluidized bed systems which treat hazardous organic compounds inherent in the operation of the system. For instance, the Foster-Wheeler Energy Corporation developed significant technology relating to the fluidized bed treatment of coal as for instance in the Daman U.S. Pat. No. 4,275,668 issued Jun. 30, 1981, the Taylor U.S. Pat. No. 4,197,086 issued Apr. 8, 1980 and other Foster-Wheeler patents of this

general time frame; however, none of the Foster-Wheeler systems and processes to the knowledge of the applicants included systems which are unvented to the atmosphere. Combustion Power Company in Palo Alto, Calif. investigated fluidized bed separation and incineration, see the Smith et al. U.S. Pat. No. 3,654,705 issued Apr. 11, 1972. A large waste incinerator was operated in Palo Alto in the 1970's and this may have been a precursor to such system. Other representative technologies in the hazardous waste disposal business include rotary kilns useful for incineration and such processes were routinely practiced throughout the United States in the 70's and 80's for incinerating waste including hazardous waste of both solid and liquid, but all of these incineration technologies involve venting off gases to the atmosphere.

Finally, there is a rotary kiln process which has been successfully used to remediate PCBs at Waukegan Harbor, Ill. and at Wide Beach, N.Y., which produces a reduced amount of off gases from the remediation, represented by the Taciuk U.S. Pat. Nos. 4,180,455, 4,280,879, 4,285,773 and 4,306,961. However, the Taciuk process still produces significant quantities of vapor which has to be treated by down stream equipment. Various technologies presently exist which combine incineration with chemical reaction in treating hazardous materials and representative examples of these are the Eggers, III U.S. Pat. Nos. 3,932,118 issued Jan. 13, 1976 and 4,040,865 issued Aug. 9, 1977, both of which relate to the pyrolysis of PCB material combined with incineration in a fluidized bed wherein  $\text{CaCO}_3$  particles are used to react with chlorine produced during the destruction of PCB to produce  $\text{CaCl}_2$ . Nevertheless, none of the technologies recited above, although representative of the presently known treatment of hazardous waste materials by fluidized beds, multiple hearth furnaces and rotary kilns, illustrate a process in which no off gases from the treatment of the hazardous waste material per se are emitted to the atmosphere.

The above quoted technologies while effective to remediate hazardous waste fall short because satisfying the local public on all aspects concerning the operations of an incinerator is often more difficult than demonstrating to the scientific community and the appropriate agencies that the emission standards can be met. The public's main concern with incinerators is the risk of toxic organic emissions or radioactive emissions. The public perceives nearby incinerators to be a risk to health imposed by the government or industry, and also a factor tending to lower property values. As a result, the siting of incinerators has become very contentious and expensive. A process that does not produce emissions, such as the inventive process described herein, may meet with greater public acceptance.

Work has been done previously to reduce or eliminate the emissions from incinerators. Stull and Golden at EG&G Rocky Flats have evaluated off-gas capture systems from a fluidized-bed oxidation unit. In the two systems evaluated, 85% of the off-gas from the fluidized bed oxidizer would be recycled with oxygen make-up, and the remaining 15% would be compressed to liquid  $\text{CO}_2$ , stored in tanks, sampled, and ultimately released. One process requires compression to 75 bar (1100 psia) at 16° C. (60° F.), and the other requires compression to 24 bar (350 psia) at -26° C. (-15° F.). Another approach was taken by Camp and Upadhye of Lawrence Livermore National Laboratory. In their proposed process, the mixed waste could be destroyed in any one of many types of incinerators with an oxidant of oxygen and recycled  $\text{CO}_2$ . The off-gases would be directly quenched with water in a venturi scrubber. Acid gases would

be removed by reacting with sodium hydroxide in a packed tower, and CO<sub>2</sub> would be removed in a second packed tower by contacting with calcium hydroxide. The remaining oxygen, CO<sub>2</sub>, water vapor, and trace gases would be recycled to the waste destructor with makeup oxygen. The solid materials in the slurries exiting the packed towers would be consolidated to moist solids, which could be buried. The Livermore process would produce a large amount of solids for burial, which was viewed by them as a disadvantage.

Still another approach is set forth in the recently issued U.S. Pat. No. 5,179,903 issued Jan. 19, 1993, to Abboud et al., which uses enriched air and high incineration temperature along with several scrubbers to treat effluents from the system.

The inventive process is designed for treating mixed wastes that have accumulated at Argonne National Laboratory (ANL) over several decades. The type of mixed waste stored at ANL that has the largest volume is scintillating counting waste, which is stored in 200 drums of 55-gal. capacity. Each drum holds 2000-4000 vials of toluene-based scintillation fluid containing radioactive materials from a wide range of projects. The vials are packed in vermiculite, which also must be treated as a mixed waste. With the proper head-end step to separate the organic liquid from the balance of the materials, this waste inventory could be treated by the inventive process hereinafter described. Also, the biological mixed waste at ANL could be treated by the proposed process, which would destroy the biological materials and separate the inorganic low-level radioactive waste for burial.

The treatment of these wastes at the ANL site is a difficult problem because ANL is located near suburban residences. Installation of a conventional incinerator would be out of the question. The inventive process and system does not release gases from the equipment during the thermal destruction of organic materials. The only products from the inventive system and process are liquid water and calcium carbonate. In one version of the invention, treating the limited quantities of ANL waste, the calcium carbonate and water produced would be mixed with cement-making materials to produce cement. This solid material would be the only product from the process.

In another version of the invention, an aqueous based CO<sub>2</sub> absorption unit is employed to remove CO<sub>2</sub> present which is used as a carrier gas along with oxygen.

The invention consists of certain novel features and a combination of parts hereinafter fully described, illustrated in the accompanying drawings, and particularly pointed out in the appended claims, it being understood that various changes in the details may be made without departing from the spirit, or sacrificing any of the advantages of the present invention.

#### BRIEF DESCRIPTION OF THE DRAWINGS

For the purpose of facilitating an understanding of the invention, there is illustrated in the accompanying drawings a preferred embodiment thereof, from an inspection of which, when considered in connection with the following description, the invention, its construction and operation, and many of its advantages should be readily understood and appreciated.

FIG. 1 is a schematic flow diagram of an embodiment of the invention;

FIG. 2 is a schematic flow diagram of another embodiment of the invention; and

FIG. 3 is a more detailed view of the embodiment of FIG. 1;

FIG. 4 is a schematic flow diagram of another embodiment of the invention showing CO<sub>2</sub> treatment;

FIG. 5 is a schematic flow diagram for absorbent treatment and CO<sub>2</sub> clean-up;

FIG. 6 is a graphical representation of the effects of oxygen concentration to the incinerator;

FIG. 7 is a graphical relationship of the CO<sub>2</sub> concentration to CO<sub>2</sub> absorption efficiency; and

FIG. 8 is a graphical representation of the relationship of CO<sub>2</sub> outlet concentration to CO<sub>2</sub> recovery efficiency.

#### DETAILED DESCRIPTION OF THE EMBODIMENT

The key feature of the inventive system and process for treating mixed and hazardous wastes is that it does not release gases during the thermal treatment operation. Referring to FIG. 1, the system 10 in which this process is practiced has a fluidized-bed reactor 11 containing a bed 12 of calcined limestone (CaO), which reacts with gases given off during oxidation of organic waste materials. Gases that will react with CaO include CO<sub>2</sub>, SO<sub>2</sub>, HCl, HBr, and other acid gases. Water vapor formed during the oxidation process is carried off with the fluidizing gas via line 13 through a ceramic candle filter 14 and removed in a condenser 15. One such filter 14 is suitable for the system 10 is a vacuum formed ceramic filter available from Industrial Filter and Pump Mfg. Co., made and operated as set forth in U.S. Pat. Nos. 4,865,629 and 4,909,813. Oxygen is added from a source 17 thereof via a line 18 to the remaining gas (mainly nitrogen), which is recirculated to the reactor 11 from a line 19 leaving the condenser 15. A controller 20 senses the CO<sub>2</sub> content in the line and controls the amount of oxygen added. Relatively pure oxygen, such as welders oxygen, is added through line 18, and the system 10 is preferably maintained with an oxygen concentration of between 20 and 70 volume percent. A blower 21 forces the recirculated dried off gases from the condenser 15 and the make-up oxygen from source 17 to the reactor 11 to maintain the fluidized bed 12 established therein.

Electric coils 22 or any suitable heating mechanism is disposed between the blower 21 and the reactor 11 to control the temperature of the bed material at start-up. After start-up, the temperature of the bed is controlled by controlling the waste feed rate and by boiler tubing (not shown) immersed in the bed, which removes heat by generating steam. Because mixed feeds often have heat value, the oxidation thereof is exothermic, so usually heat has to be removed after start-up rather than added; however, coil 22 could be used to add heat if required. A waste feed 23, a lime or calcined limestone inlet 24 and a spent bed or ash outlet 25 are provided, all such fixtures being well known in the fluidized bed art. From the condenser 15 water is transferred via a line 26 to a collector or to treatment such as to an activated carbon bed 27. The activated carbon from the bed 27 when loaded can be introduced into the bed 12 for incineration to ash. Nitrogen is bled from line 19 by a pump 28 and sent via a line 29 to a container 30 therefor.

Thus, for most organic waste materials, there is no net production of gas by the reactions occurring within the equipment. A small amount of nitrogen might need to be collected as a result of (a) nitrogen impurity contained in the oxygen feed, (b) leakage of gas into the equipment through flanges, or (c) nitrogen released during the destruction of some organic compounds such as amines. Moreover, the nitrogen thus collected can be used to clean the ceramic candle filters by blow back mechanism, not shown. The excess gas, mainly nitrogen, is released after treatment and analysis.

Referring to FIG. 2, the most flexible arrangement is shown in system 50 and involves separating the processor into two separate units: an oxidizer 51 and a carbon dioxide sorber 71. The oxidizer 51 can be operated at high temperatures (600°–900° C.) to ensure complete oxidation, whereas the sorber 71 can be operated at a lower temperature (500° C.) appropriate for CO<sub>2</sub> sorption with a temperature range of from about 500° C. to about 750° C. being acceptable and a range of 500° C. to 700° C. being preferred. As is known by equilibrium data, CaCO<sub>3</sub> is stable at the operating condition in the sorber, but Ca(OH)<sub>2</sub> is not. In this process, the oxidizer 51 could be (a) a fluidized bed with a mixture of sand and lime for bed material, (b) a slagging combustor, or (c) various conventional incinerators such as a rotary kiln.

The oxidizer 51 as previously indicated, may be of any type, but the off gas from the oxidizer 51 will leave through a line 53 after passing through a filter 54 which may be of the same type previously disclosed, that is a ceramic candle filter. The off gases from the oxidizer 51 flow into the sorber 71 which is provided with calcined limestone through an inlet 72. Gases from the sorber 71 leave via a line 55 after passing through a high temperature filter 56 which also may be a ceramic candle filter. The line 55 leads to a condenser 57 which is operated at a reduced temperature, such as in the range of 40° and 80° C. in order to condense a portion of the water in the off gas from the sorber. It will be understood that the condenser 57 like the condenser 15 may be operated at any temperature below the condensation temperature, the precise temperature being one of choice and depending on the economies of system. Condensed water is removed from the condenser through line 58 to a waste water treatment or storage facility 59 which may be an activated carbon bin. Similar to the system 10 when the carbon in the bed 59 is full of absorbed materials, it may be dumped into the oxidizer 51 and be converted to ash resulting in no additional material to be treated. Dried off gases flow out of the condenser 57 in the line 60 where nitrogen is bled off via a pump 62 and transported by a line 63 to a storage container 64 therefor. The nitrogen may be stored under pressure and used along with blow back mechanism (not shown) to clean the filters 54 and 56 by back flushing.

Oxygen from a source 65 thereof may be added to the dried gas in the line 60 by a controller 66 which senses the oxygen concentration in the dried off gases leaving the condenser 57 and supplies oxygen such that the total oxygen concentration in the gas flowing to the oxidizer is in the range of between about 20 volume and 70 volume percent. The oxygen source 65 is preferably relatively pure oxygen such as welders oxygen which is greater than 99.5% pure. A blower 67 is interposed in the line 60 so as to force the dried off gases into the oxidizer at sufficient velocity, these velocities depending on the type of oxidizer used. If the oxidizer is a fluidized bed, obviously then the velocity of the gas will have to be sufficient to fluidize the particulate material inside the oxidizer 51. An electrical heating mechanism 68 is interposed on the line between the blower 67 and the oxidizer 51 in order to add heat to the system 50 at system start-up, because of the unusually high oxygen content of the system 50, additional heat is usually not required even if the waste material being incinerated has a low heating value.

The oxidizer 51 is provided with an inlet 69 for the spent sand and sorber line from the fluidized bed sorber 71 and waste inlet 70 for the introduction of the organic waste material to be burned. Like the fluidized bed reactor 11, the oxidizer is provided with an ash outlet 73. The fluidized bed sorber 71 is provided with an outlet 74 through which calcium carbonate which is formed during the intimate

mixing of the off gas from the oxidizer with the calcine limestone in the sorber 71 is transmitted to a holding tank not shown, and from there to a calciner 75 for regeneration or to some other treatment center for disposal. If the calcium carbonate formed in the sorber is transmitted to a calciner, it is preferred that the calciner be operated at a temperature of about 950° C. which is a sufficient temperature to convert the calcium carbonate into CO<sub>2</sub> which exits the calciner through a line 76 and lime which exits the calciner 75 through a line 77 and is returned to the sorber 71 through the inlet 72. As indicated in FIG. 2, the infeed to the calciner comes from the calcium carbonate produced in the sorber 71 and a portion thereof can be sent to the oxidizer to be converted to ash so as to permit fresh lime or calcined limestone to be added to the system as required and as desirable.

In all cases, the gas from the sorber 71 is cooled to condense the water and recirculated to the oxidizer 51 with sufficient oxygen to support combustion. Lime is continuously fed to the sorber bed 71a through line 72 and continuously withdrawn through an overflow pipe (not shown). The pressure at the outlet of FIG. 2 circulating blower will be controlled at slightly less than atmospheric pressure to assure that any leaks in the system do not result in the escape of hazardous material.

If all of the reaction products are converted to cement, as intended for the ANL wastes, the total volume of the waste material might be somewhat larger than the initial organic waste volume because of the conversion of the carbon in the organic material to CaCO<sub>3</sub>. This moderate increase in volume is not important in treating the ANL wastes because the total waste volume is not large and more serious problems than the waste volume are solved by the new processing scheme. This approach may also be practical for treatment of certain mixed and hazardous wastes found at other sites.

For medical wastes and other organic wastes generated at moderate rates on a site, it may be inappropriate to convert the products of the inventive process to cement. The spent lime could be analyzed to demonstrate virtual complete destruction of the organic matter and then trucked to a cement manufacturer (which may also be the supplier of the lime) for inclusion in the products of that manufacturer.

Alternatively, the volume of the products from the inventive process and of the lime supplied as reactant may be greatly reduced yet retain the main features of the process. To reduce these volumes, spent lime (mainly calcium carbonate) would be calcined in a separate unit to decompose the CaCO<sub>3</sub>, recover the lime, and release carbon dioxide (upper right-hand corner of FIG. 2). The most energy-efficient form of this process would be to transfer the hot bed material 71a from the sorber 71 to the calciner 75 without cooling. To facilitate the reuse of the spent lime 69 leaving the sorber 71, it would be advantageous to add lime to the oxidizer 51 if acid gases such as SO<sub>2</sub>, HCl, or HBr are being produced. This will result in the retention of sulfur and the halogens in the oxidizer ash 73. The source of the lime for the oxidizer 51 would be a small side stream 74 taken from the spent lime in the sorber 71. Thus, the only solid waste stream from the process would be the ash 73 from the oxidizer 51. The volume of ash per unit mass of waste destroyed would be about the same as for a standard fluidized-bed incinerator to which limestone is added to retain the acid-gas anions with the ash.

The division of the (a) destruction of the organic material and (b) decomposition of the calcium carbonate into separate steps carried out in different equipment greatly reduces

the likelihood of the release of toxic materials from that associated with standard incinerators. Only gases enter the sorber 71, and these are almost entirely free of the hazardous organics fed to the oxidizer 51. Only a small fraction of the organic material that escapes the oxidizer 51 will be retained on the hot spent lime 74 released from the sorber 71. Most of the gas, including unreacted organics, will pass through the sorber 71 and be recirculated to the oxidizer 51. To minimize the amount of organic material released from the calciner 75, it must be indirectly heated and thus involve no air or sweep gas addition. However, it may be practical to add a small stream of gas from the inert gas collection tank 64 (which may be treated and sampled if desired) to dispose of the small amount of nitrogen entering the process, primarily as an impurity with the oxygen supply. Under these conditions of restricted gas addition, no gas is released from the calciner 75 if the temperature inadvertently drops below the minimum calcining temperatures of 800°–900° C. This approach results in long retention times at high temperatures for destroying the tiny fraction of organic gases which may be clinging to the spent lime. The off-gas 76 from the calciner 75 as operated above, would be more than 90% carbon dioxide with small amounts of oxygen and nitrogen, even with the addition of gas from the inert gas collection tank as proposed above. Its volume per unit of waste destroyed would be about 10% of that from a conventional incinerator. The off-gas treatment system required for this carbon dioxide stream 76 would consist of cooling and filtering equipment, and should be comparatively inexpensive.

If the waste to be treated contains hazardous metals or radioactive solids, it may be appropriate to vitrify the ash 73 from the oxidizer 51. Alternatively, the oxidizer 51 may be operated at an enriched oxygen level to produce a glassy slag directly. Operating at high oxygen levels is easily done in the inventive process because the oxidant 65 added to the process is pure oxygen.

Additional tests will be carried out with a single processing unit 100, as shown in FIG. 3. The main processing unit for these studies is a fluidized-bed reactor 101 used previously for studying fluidized-bed combustion of coal. This fluidized-bed reactor has an internal diameter of 15.2 cm (6-in.) and in the previous projects was equipped for continuous feed 102 of limestone (for removal of sulfur) and continuous feed of powdered coal through inlet 103 or inlet 104, now adapted for mixed waste, solids or slurries through inlet 103 and liquids through 104.

Above the fluidized bed reactor 101 is a ceramic candle filter assembly 105 which leads via a line 106 to a water condenser 107 into a condensate separator 108. A gas recycle blower 110 will recirculate the gases through the system, there also being provided a preheater 111, which may be either electric or of another type but in any event, constructed and arranged so as not to add additional gases to the system. Make-up oxygen enters the system through an inlet 112 and is obtained from a source of relatively pure oxygen as before described. The sensors and controllers previously described with respect to FIGS. 1 and 2 will be included in this system but are not here included for brevity. The spent lime exits the fluidized reactor through an outlet 113 and may be recirculated, if necessary, to a calciner not shown and ash exits the system from an outlet 114 and may be treated as previously described. The waste water collector 115 may be used as previously described with respect to the systems of FIGS. 1 and 2 and may be sent off-site for treatment or for use in converting the waste to cement as previously described.

There is also provided a waste gas outlet conduit 116 which can be connected to a storage facility, not shown. Although the system or processing unit 100 illustrated in FIG. 3 was previously used for processing coal, it is clear that the system with some modifications can easily be used to conduct the necessary test to verify the parameters of the subject invention.

In the initial experiments on waste burning, the unit 110 will be operated with once-through gas flow and with toluene fed as a model waste compound. The bed temperature will be raised to the ignition temperature by preheating the fluidizing/combustion air stream. Once the bed is at the ignition temperature, toluene will be injected into the fluidized bed, and the experimental conditions of bed temperature and the rates of toluene and lime feed will be established. The toluene and lime will be fed to the processor continuously, and bed material will continuously overflow into a closed collection vessel. Bed temperature will be maintained by controlling the toluene feed rate and by employing an in-bed heat exchanger. The planned range of test conditions is summarized in Table I.

TABLE I

Planned Test Conditions	
Parameter	Value
Liquid feed	Toluene
Liquid feed rate, kg/h	0.10–0.36
Lime (CaO) feed rate, kg/h	1.5–2.3
CaO/C mole feed ratio	1.1–1.5
System pressure, bar	1.0
Bed temperature, °C.	600–700
Fluidizing velocity, m/s	0.76–0.91

The objective of these initial tests will be to measure and verify basic process performance parameters, such as the efficiency of toluene destruction in a single pass through the fluidized bed, the extent of the conversion of CaO to CaCO<sub>3</sub> as a function of the toluene-to-lime feed ratio, and the CO<sub>2</sub> concentration in the off gas. It will also be important to verify in these early tests that the reactive lime collected in the bed overflow is not contaminated by organic material.

Modifications to the facility have been designed and equipment procurements initiated to convert the existing fluidized-bed reactor 101 to a reactor of the type shown in system 10 with gas recirculation. A key component in the modified facility will be a candle filter assembly 105 for filtering the dust from the combustion gases and returning the solids to the fluidized bed in reactor 101. Other components include a water condenser 107 and condensate separator 108 to remove water from the gas stream, a gas recycle blower 110, and oxygen addition equipment 112, all as previously described.

The present reactor system 100 shows a slight tendency for the pressure to rise as a result of nitrogen contained as an impurity in the oxygen supplied and in air leaking into the equipment through flanges. To control the pressure at the outlet of the circulating blower to slightly below atmospheric pressure, gas will be withdrawn through line 116 by a compressor and stored at elevated pressure in a holding tank. This relatively small amount of gas may be analyzed and, if necessary, treated prior to release to the environment.

When the modifications have been completed, experiments will proceed using toluene and carbon tetrachloride as model compounds to demonstrate the destruction of organic materials without release of gases.

To aid in assessing the practicality of the proposed process, a calculation was made for the system 10. The compositions and the content of the inlet and outlet gas streams and the inlet and outlet bed material streams were calculated. The calculation of the bed densities and volumes is based on our experience in using lime in the fluidized-bed reactor for coal-burning experiments. In those experiments, it was found that the lime particles obtained by calcining limestone have a calcium density of 0.024 g-mol/cm<sup>3</sup>. The particles retain their size throughout the process while changing composition and density.

Some of the key parameters are shown in Table II. These sets of calculations were made for a liquid feed mixture of toluene-20 wt. % carbon tetrachloride. Both of these constituents of the feed mixture are contained in Argonne's mixed waste inventory, and calculations were made to determine how the process would handle chlorinated hydrocarbons, a common type of hazardous and mixed-waste constituent. The first two columns of values in Table II are for the experimental reactor, which has an inside diameter of 15.2 cm (6 in.). The results shown in the first column are for a feed rate just high enough to maintain the operating temperature of the reactor without cooling the bed. The calculations in the second column are for the maximum feed rate, which was taken to be that which required an oxygen concentration of 70% for the inlet fluidizing gas, which nearly coincides with the rate calculated for the maximum practical amount of cooling tubing within the bed of the experimental reactor. The experimental reactor has a bed depth of only 91 cm (3 ft.).

Calculations have been made for a large-scale reactor in the right-hand column of Table II. In scaling up the reactor, the program calculates the height of the expanded fluidized bed to be proportional to the 0.4 power of the diameter. For this reactor of 5 m-diameter, the height is 3.7 m. This configuration results in an outlet gas pressure of only 0.612 bar, indicating that the bed depth is near the practical limit. This deep bed results in a long retention time for the bed material, 68.5 minutes, which should facilitate achieving the assumed extent of lime reaction of 70%. From calculations, it is apparent that the unvented processor is better adapted to processing large throughputs of chlorinated hydrocarbons than fuel-like materials such as toluene. The chlorinated hydrocarbons not only produce less heat but also require less oxygen.

A problem in treating chlorinated hydrocarbons is the formation of calcium chloride, which may result in a tendency to particle agglomeration. Two solutions to this problem are proposed. One is to design a separate oxidizer 51 and sorber 71, as shown in FIG. 2. The other is to blend the chlorinated hydrocarbon with other hydrocarbons to reduce the concentration of calcium chloride in the bed material. It has been calculated that for a mixture of toluene-20 wt. % carbon tetrachloride, the bed material at equilibrium would contain only about 4% calcium chloride. Such a low concentration of calcium chloride is not likely to result in bed caking.

TABLE II

System Parameters	Calculated Performance of Unvented Processor		
	Experimental Reactor	Large Scale Reactor	
	No Bed Cooling	Maximum Rate	Maximum Rate
10 Reactor internal diameter, cm	15.2	15.2	500
Control temperature, °C.	700	700	700
Feed Composition, wt %			
Toluene	80	80	80
Carbon tetrachloride	20	20	20
15 Feed rate, kg/h	0.991	5.84	6.320
Oxygen reaction requirement, g-moles/min	1.31	7.73	8.360
Bed Material Parameters			
Expanded bed height, cm	91	91	370
20 Volume of boiler tubing within bed, liters	0	2.61	3.180
Ca density of particles, g-moles/cc	0.024	0.024	0.024
Percent CaO reacted	70	70	70
Feed rate, kg/h	5.14	30.2	32.700
Discharge Rate, kg/h	7.98	47.0	50.900
Bed Retention time, min	104	14.9	68.5
25 Inlet Gas Conditions			
Temperature, °C.	40	40	40
Pressure (absolute), bars	0.988	0.988	0.988
Oxygen concentration, vol %	20.2	70.0	70.0
30 Linear flow rate at reactor temp., ft/sec	3.29	2.25	3.08
Fraction of carbon dioxide reacted, %	90	90	90
Outlet Gas Conditions			
Temperature, °C.	700	700	700
35 Pressure (absolute), bars	0.846	0.846	0.612
Oxygen concentration, vol. %	10	10	10
Linear flow rate at reactor temp., ft/sec	3.29	2.25	3.08
Reactor Heat Balance, (25° C. basis), kW			
40 Heat entering with fluidized gas	0.091	0.094	102
Heat from burning toluene mixture	8.93	52.5	56.800
Heat from time reactions			
Reaction of CO <sub>2</sub> from toluene	3.0	17.7	19.200
Reaction of CCl <sub>4</sub>	0.3	1.73	1.870
45 Heat leaving with fluidizing gas	4.05	3.1	3.370
Heat leaving with bed material	1.56	9.18	9.950
Heat losses through reactor wall	6.67	6.67	78.3
Heat removed by cooling coil, kW	0	53	64.600

50 Industrial and governmental installations produce many types of hazardous wastes requiring oxidation of organic material during treatment. Some liquid and solid wastes have very high heating values, while others require the addition of an auxiliary fuel to support combustion. Mixed wastes are particularly difficult to treat by standard incineration processes because the emissions may contain radioactive volatile matter or fine particles that escape filtration of the gaseous effluent. These problems are greatly alleviated by the inventive system and process, even for the version of the system and process where the spent lime is regenerated, because of the isolation of the lime during calcining from both the gases formed on destruction of the organic material and the ash which contains radioactive solids.

55 The need for pure oxygen as the oxidant for the inventive process is a cost factor that affects the types of wastes that can be economically treated. The combined effects of the cost of oxygen and the avoidance of emissions result in the following types of wastes being favored for treatment:

60

65

## 11

Industrial, military, and DOE wastes containing chlorinated hydrocarbons. Such wastes have low oxygen requirements for destruction.

Solid and liquid mixed wastes. These are particularly hazardous to destroy by standard incineration.

Hospital wastes. These are generated near residential property, are not easily trucked away, and have only a moderate oxygen requirement.

The oxidizer 51 and sorber 71 can be combined into one unit, a fluidized bed containing lime, for destruction of liquid combustible wastes. For most other wastes, including all solids and sludges and liquids having high chlorine, bromine, or sulfur content, the oxidizer and sorber would be constructed as two separate units.

The oxidizer 51 and sorber 71, or the combined unit 11 with these functions, will be constructed primarily of carbon steel and lined with refractory materials, as is typically done in the construction of commercially available boilers and furnaces. To construct a system for practicing the inventive process, the carbon dioxide sorber, water condenser, and recirculation equipment would be installed instead of the extensive exhaust treatment system of a conventional incinerator. For the system in which the lime is regenerated and recycled on site, the off-gas from the calcining unit would have only 10% of the volume of the off-gas from a conventional incinerator and would require only cooling and filtration to remove solids. On-line monitoring, sampling, and analytical costs are likely to be lower for the inventive process than for an incinerator.

The oxygen requirements for the combustor is known to be a major cost item. A preliminary analysis indicates that the cost of the oxygen will be \$50 to \$300 per ton of waste, depending on the oxygen requirement of the particular waste treated. The oxygen cost will be offset to some extent by the higher throughput available for an oxidizer if supplied with gas at high oxygen concentration.

As shown particularly in FIGS. 4 and 5, a delayed release process having the following characteristics is disclosed.

1. The reaction products, CO<sub>2</sub> and water, which are produced in the incinerator and contained in the exhaust gas are absorbed in aqueous solutions.
2. The remaining gas is recycled to the incinerator with addition of oxygen.
3. The liquid absorbent containing the CO<sub>2</sub> and water is purified, analyzed and stored.

## 12

4. If the stored absorbent passes the analytical test, the CO<sub>2</sub> and water are released, otherwise the absorbent is recycled to purification.

The gas that would normally be released up the stack in prior art processes is cooled in a condenser to remove the moisture added in the water quenching steps. The cool, relatively dry, gas is returned to the incinerator with oxygen addition. The carbon dioxide is removed in a sidestream. The use of a sidestream, rather than absorption from the main stream, results in a high CO<sub>2</sub> concentration at the inlet of the CO<sub>2</sub> absorber and, therefore, reduces the absorber size and cost.

More detail on the CO<sub>2</sub> removal, purification, and release is shown in FIG. 5. The CO<sub>2</sub>-rich absorbent leaving the absorption tower is filtered to remove particles transferred from the off-gas and any precipitates. The liquid absorbent from the filter is purified of any organic carbon transferred from the off-gas by means of a partial gas release stage. CO<sub>2</sub> and water vapor given off in this stage would strip organic materials of low solubility from the solution. The gas thus given off would be combined with the off-gas from the CO<sub>2</sub> absorber and the combined gas (Stream R in FIG. 4) would be returned to the main loop which returns gas to the incinerator. The purified CO<sub>2</sub> absorbent would be continuously monitored for organic carbon as it leaves the purification system and enters holding tanks. One process for liquid holdup is that each of two holding tanks would have a capacity of about 10 minutes and that these tanks would alternate in filling, holding, and then dumping their contents to a feed tank that would feed the gas release stage. Liquid absorbent that did not pass the test for organic carbon would be recycled to the inlet of the filter as shown in FIG. 5. In the gas release stage, both the reaction product CO<sub>2</sub> and water which are generated in the incinerator would be released by raising the temperature or lowering the pressure. The regenerated absorbent would be recycled to the CO<sub>2</sub> absorber.

Material balance calculations were made for six cases and the results are shown in the spreadsheet of Table 3 for a waste feed rate of one metric ton per hour and 20% excess oxygen in the gas entering the incinerator. Various levels were considered for the other key variables including oxygen concentration to the incinerator, nitrogen concentration in the oxygen supply, the rate of release of gas to remove nitrogen, and the CO<sub>2</sub> removal efficiency. These variables affect the percentage of recirculated gas that is diverted to the absorber and the concentration of CO<sub>2</sub> in that stream.

TABLE 3

<u>DELAYED RELEASE FLOWSHEET - CO<sub>2</sub> ABSORPTION FROM SIDE LOOP</u>						
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
<u>Calculation Summary</u>						
<u>Key Variables</u>						
Waste feed rate to incinerator, metric tons/hr	1.0	1.0	1.0	1.0	1.0	1.0
Excess oxygen to incinerator, %	20	20	20	20	20	20
Oxygen concentration to incinerator, vol %	20	40	40	40	40	40
Nitrogen concentration in oxygen supply, %	0.50	0.50	0.50	0.50	0.10	0.10
Pressure control (N <sub>2</sub> bleed) rate, % of off-gas	0.30	0.30	0.30	0.50	0.30	0.10
CO <sub>2</sub> removal efficiency, %	90	90	80	60	70	70
Side steam flow to absorber (S/C), %	16.6	46.6	59.5	46.4	47.2	56.2
<u>Waste Feed Material</u>						
Carbon fraction, %	30	30	30	30	30	30
Hydrogen-to-carbon atom fraction (dry basis)	1.6	1.6	1.6	1.6	1.6	1.6

TABLE 3-continued

	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
<u>DELAYED RELEASE FLOWSHEET - CO2 ABSORPTION FROM SIDE LOOP</u>						
Chlorine-to-carbon atom fraction	0.1	0.1	0.1	0.1	0.1	0.1
Water in waste, wt %	10.0	10.0	10.0	10.0	10.0	10.0
Added Fuel (Methane), wt % of Waste	8.0	6.0	6.0	6.0	6.0	6.0
<u>Gas Stream Conditions</u>						
Off-gas from incinerator (A), kg/hr	10,700	4,830	4,700	4,960	5,110	4,900
Gas to CO2 Absorber						
<u>Flow rate</u>						
kg/hr	1,660	1,940	2,400	1,990	2,100	2,380
Cfm at 50 C	654	818	1,044	815	829	986
<u>CO2 concentration</u>						
Weight %	87.4	72.3	65.7	78.7	85.4	75.8
Volume %	78.7	60.8	53.5	68.2	76.6	64.8
<u>Gas from CO2 Absorber</u>						
<u>Flow rate</u>						
kg/hr	354	678	1,140	739	843	1,117
Cfm at 50 C	190	370	597	370	385	539
<u>CO2 concentration</u>						
Weight %	41.0	20.7	27.7	42.5	63.8	48.5
Volume %	27.0	13.4	18.7	30.0	49.6	35.6
<u>Calculation Details</u>						
Basis: 1 kg-atom/hr carbon						
Excess Oxygen, %	20	20	20	20	20	20
Oxygen Conc. to Incinerator, vol %	20	40	40	40	40	40
CO2 Removal Efficiency, %	90	90	80	80	70	70
Pressure Control Rate, kg/hr	1.0702	0.5038	0.4904	0.8625	0.5328	0.1703
Pressure control ratio (PC/A), %	0.30	0.30	0.30	0.50	0.30	0.10
Side steam flow to absorber (S/C), %	16.61	46.56	59.46	46.36	47.23	56.20
<u>Feed Material</u>						
Waste feed rate to incinerator, metric tons/hr	1.0	1.0	1.0	1.0	1.0	1.0
Carbon fraction, %	30	30	30	30	30	30
Hydrogen-to-carbon atom fraction (dry basis)	1.6	1.6	1.6	1.6	1.6	1.6
Chlorine-to-carbon atom fraction	0.1	0.1	0.1	0.1	0.1	0.1
Water in waste, wt %	10	10	10	10	10	10
Added fuel (methane), wt % of waste	8	6	6	6	6	6
Total carbon, kg/hr	360	345	345	345	345	345
Hydrogen (dry basis), kg/hr	60	55	55	55	55	55
Chlorine, kg/hr	89	89	89	89	89	89
Water, kg/hr	100	100	100	100	100	100
<u>Burnable waste, water and fuel rates converted to basis of 1.0 kg-atoms/hr of carbon</u>						
<u>Rates, kg-atoms/hr</u>						
Carbon (calculation basis)	1.00	1.00	1.00	1.00	1.00	1.00
Hydrogen (organic)	2.00	1.91	1.91	1.91	1.91	1.91
Chlorine	0.08	0.09	0.09	0.09	0.09	0.09
Water, (kg-moles/hr)	0.19	0.19	0.19	0.19	0.19	0.19
Total	3.27	3.19	3.19	3.19	3.19	3.19
<u>Rates, kg/hr</u>						
Carbon (calculation basis)	12.00	12.00	12.00	12.00	12.00	12.00
Hydrogen (organic)	2.00	1.91	1.91	1.91	1.91	1.91
Chlorine	2.96	3.09	3.09	3.09	3.09	3.09
Water	3.33	3.48	3.48	3.48	3.48	3.48
Total	20.29	20.48	20.48	20.48	20.48	20.48
<u>Stream F to Incinerator</u>						
<u>Rate, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	56.80	55.93	55.93	55.93	55.93	55.93
N2	15.86	23.58	31.89	15.10	5.45	18.94



TABLE 3-continued

<u>DELAYED RELEASE FLOWSHEET - CO2 ABSORPTION FROM SIDE LOOP</u>						
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
H2O	16.42	7.17	6.97	7.36	7.66	7.35
CO2	247.35	60.76	48.21	73.64	88.06	67.64
<u>Total</u>	336.43	147.45	143.00	152.03	157.11	149.85
<u>Rate, moles/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	1.78	1.75	1.75	1.75	1.75	1.75
N2	0.57	0.84	1.14	0.54	0.19	0.68
H2O	0.91	0.40	0.39	0.41	0.43	0.41
CO2	5.62	1.38	1.10	1.67	2.00	1.54
<u>Total</u>	8.88	4.37	4.37	4.37	4.37	4.37
<u>Stream A from Incinerator, kg/hr</u>						
HCl	3.04	3.17	3.17	3.17	3.17	3.17
O2	9.47	9.32	9.32	9.32	9.32	9.32
N2	15.86	23.58	31.89	15.10	5.45	18.94
H2O	37.00	27.09	26.88	27.27	27.57	27.26
CO2	291.35	104.76	92.21	117.64	132.06	111.64
<u>Total</u>	356.72	167.93	163.47	172.51	177.58	170.33
<u>Check Total</u>	356.72	167.93	163.47	172.51	177.58	170.33
<u>Partial Water Quench</u>	163.73	77.08	75.03	79.18	81.51	78.18
<u>Rate, kg/hr</u>						
<u>Stream B to Scrubbing, kg/hr</u>						
HCl	3.04	3.17	3.17	3.17	3.17	3.17
O2	9.47	9.32	9.32	9.32	9.32	9.32
N2	15.86	23.58	31.89	15.10	5.45	18.94
H2O	200.73	104.16	101.92	106.45	109.09	105.44
CO2	291.35	104.76	92.21	117.64	132.06	111.64
<u>Total</u>	520.45	245.01	238.51	251.69	259.10	248.51
<u>Stream C from Condenser</u>						
<u>Rate, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	9.47	9.32	9.32	9.32	9.32	9.32
N2	15.86	23.58	31.89	15.10	5.45	18.94
H2O	16.67	7.25	7.02	7.48	7.73	7.36
CO2	291.35	104.76	92.21	117.64	132.06	111.64
<u>Total</u>	333.34	144.91	140.44	149.54	154.56	147.26
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	2.84	6.43	6.64	6.23	6.03	6.33
N2	4.76	16.28	22.71	10.10	3.53	12.86
H2O	5.00	5.00	5.00	5.00	5.00	5.00
CO2	87.40	72.29	65.66	78.67	85.44	75.81
<u>Total</u>	100.00	100.00	100.00	100.00	100.00	100.00
<u>Oxygen Stream</u>						
Nitrogen Concentration, %	0.50	0.50	0.50	0.50	0.10	0.10
<u>Rate, kg/hr</u>						
O2	47.48	46.70	46.68	46.75	46.69	46.63
N2	0.24	0.23	0.23	0.23	0.05	0.05
<u>Total</u>	47.71	46.94	46.91	46.99	46.74	46.68
<u>Stream P, Pressure Control</u>						
<u>Rate, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	0.14	0.09	0.07	0.15	0.08	0.02
N2	0.24	0.23	0.23	0.23	0.05	0.05
H2O	0.25	0.07	0.05	0.12	0.07	0.02
CO2	0.44	0.10	0.14	0.37	0.34	0.08
<u>Total</u>	1.07	0.50	0.49	0.86	0.53	0.17

TABLE 3-continued

	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
<u>DELAYED RELEASE FLOWSHEET - CO2 ABSORPTION FROM SIDE LOOP</u>						
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	13.31	18.41	13.98	16.82	15.01	13.49
N2	22.29	46.58	47.83	27.24	8.77	27.40
H2O	23.43	14.31	10.53	13.49	12.44	10.65
CO2	40.96	20.69	27.66	42.45	63.78	48.46
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream D, Bypass of Side Loop</u>						
<u>Rates, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	7.89	4.98	3.78	5.00	4.92	4.08
N2	13.22	12.60	12.93	8.10	2.88	8.30
H2O	13.90	3.87	2.85	4.01	4.08	3.23
CO2	242.95	55.99	37.38	63.10	69.69	48.90
Total	277.97	77.45	56.93	80.21	81.57	64.50
Total (check)	277.97	77.45	56.93	80.21	81.57	64.50
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	2.84	6.43	6.64	6.23	6.03	6.33
N2	4.76	16.28	22.71	10.10	3.53	12.86
H2O	5.00	5.00	5.00	5.00	5.00	5.00
CO2	87.40	72.29	65.66	78.67	85.44	75.81
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream E, Recycle Gas</u>						
<u>Rates, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	9.32	9.23	9.25	9.18	9.24	9.30
N2	15.62	23.35	31.65	14.86	5.40	18.89
H2O	16.42	7.17	6.97	7.36	7.66	7.35
CO2	247.35	60.76	48.21	73.64	88.06	67.64
Total	288.71	100.51	96.08	105.04	110.37	103.18
Total (check)	288.71	100.51	96.08	105.04	110.37	103.18
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	3.23	9.18	9.63	8.74	8.37	9.01
N2	5.41	23.23	32.94	14.15	4.89	18.31
H2O	5.69	7.14	7.25	7.01	6.94	7.12
CO2	85.67	60.45	50.17	70.11	79.79	65.56
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream R*, Outlet from CO2 Absorber</u>						
<u>Rates, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	1.57	4.34	5.54	4.32	4.40	5.24
N2	2.63	10.98	18.96	7.00	2.57	10.64
H2O	2.77	3.37	4.18	3.47	3.65	4.14
CO2	4.84	4.86	10.97	10.91	16.71	18.82
Total	11.82	23.57	39.65	25.70	29.34	38.84
Total (check)	11.82	23.57	39.65	25.70	29.34	38.84
<u>Rates, mole/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	0.05	0.14	0.17	0.14	0.14	0.16
N2	0.09	0.39	0.66	0.25	0.09	0.38
H2O	0.15	0.19	0.23	0.19	0.20	0.23
CO2	0.11	0.11	0.25	0.25	0.43	0.43
Total	0.41	0.83	1.33	0.83	0.86	1.20
CO2 volume fraction, %	27.02	13.42	18.72	30.03	49.59	35.60

TABLE 3-continued

<u>DELAYED RELEASE FLOWSHEET - CO2 ABSORPTION FROM SIDE LOOP</u>						
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	13.31	18.41	13.96	16.82	15.01	13.49
N2	22.29	48.58	47.83	27.24	8.77	27.40
H2O	23.43	14.31	10.53	13.49	12.44	10.65
CO2	40.96	20.69	27.66	42.45	63.78	48.46
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream R, Return from Side Loop</u>						
<u>Rates, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	1.43	4.25	5.47	4.18	4.32	5.22
N2	2.40	10.75	18.73	6.76	2.53	10.60
H2O	2.52	3.30	4.12	3.35	3.58	4.12
CO2	4.40	4.77	10.83	10.54	18.37	18.74
Total	10.75	23.07	39.16	24.83	28.80	38.67
<u>Percentage</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	13.31	18.41	13.98	16.82	15.01	13.49
N2	22.29	46.58	47.83	27.24	8.77	27.40
H2O	23.43	14.31	10.53	13.49	12.44	10.65
CO2	40.96	20.69	27.66	42.45	83.78	46.46
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream S Supply to Side Loop</u>						
<u>Rates, kg/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	1.57	4.34	5.54	4.32	4.40	5.24
N2	2.63	10.98	18.96	7.00	2.57	10.64
H2O	2.77	3.37	4.18	3.47	3.65	4.14
CO2	48.40	48.77	54.83	54.54	62.37	62.74
Total	55.38	67.47	83.51	69.33	73.00	82.76
<u>Rates, mole/hr</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	0.05	0.14	0.17	0.14	0.14	0.16
N2	0.09	0.39	0.68	0.25	0.09	0.38
H2O	0.15	0.19	0.23	0.19	0.20	0.23
CO2	1.10	1.11	1.25	1.24	1.42	1.43
Total	1.40	1.82	2.33	1.82	1.85	2.20
<u>CO2 volume fraction, %</u>						
HCl	0.00	0.00	0.00	0.00	0.00	0.00
O2	2.84	6.43	6.64	6.23	6.03	6.33
N2	4.76	16.28	22.71	10.10	3.53	12.86
H2O	5.00	5.00	5.00	5.00	5.00	5.00
CO2	87.40	72.29	65.66	78.67	85.44	75.81
Total	100.00	100.00	100.00	100.00	100.00	100.00
<u>Stream NaOH, kg/hr</u>						
<u>Salt and Condensate, kg/hr</u>						
<u>HCl in salt</u>						
H2O	184.07	96.92	94.90	98.98	101.36	98.08
Total	187.11	100.09	98.07	102.15	104.53	101.25
<u>CO2 Absorbed</u>						
<u>Rate, kg/hr</u>						
Removal Efficiency, %	90.00	90.00	80.00	80.00	70.00	70.00

TABLE 3-continued

<u>DELAYED RELEASE FLOWSHEET - CO<sub>2</sub> ABSORPTION FROM SIDE LOOP</u>						
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
<u>Summary of Input and Output Streams</u>						
<u>Input</u>						
Waste Feed Elements (C + H + Cl + H <sub>2</sub> O)	20.29	20.48	20.48	20.48	20.48	20.48
Oxygen Feed	47.71	46.94	46.91	46.99	46.74	46.68
Quench Water	163.73	77.08	75.03	79.18	81.51	78.18
Total	231.74	144.49	142.43	146.65	148.72	145.34
<u>Output</u>						
H <sub>2</sub> O and HCl by Scrubbing	187.11	100.09	98.07	102.15	104.53	101.25
CO <sub>2</sub> by Absorbent Contact	43.56	43.90	43.86	43.63	43.66	43.92
Pressure Control Stream	1.07	0.50	0.49	0.86	0.53	0.17
Total	231.74	144.49	142.43	146.65	148.72	145.34

The effects of some of the key variables are shown graphically in FIGS. 6 and 7. The effect of the oxygen concentration in the gas entering the incinerator on the CO<sub>2</sub> concentration to the absorber is shown in FIG. 7. For all concentrations of interest, the concentration of CO<sub>2</sub> to the absorber will be considerably higher than for most processes in which CO<sub>2</sub> is absorbed. The use of an oxygen concentration entering the incinerator of at least 40% is beneficial in that the flow rate of off-gas from the incinerator is much reduced from that associated with the use of air for the combustion gas (FIG. 6). In FIG. 7, the effects of the CO<sub>2</sub> absorption efficiency are illustrated. The absorption efficiency takes into account the CO<sub>2</sub> which is driven out during the purification step as this CO<sub>2</sub> is returned to the incinerator loop as a part of Stream E in FIG. 4. As the CO<sub>2</sub> absorption efficiency increases, the CO<sub>2</sub> concentration to the absorber increases and the rate of flow in the sidestream to the absorber decreases in absolute terms and as a percent of Stream C (FIG. 7).

The delayed release system has several advantages over standard off-gas treatment systems. Normally, the level of toxic hydrocarbons released from a well-operating incinerator are very low. However, torn filters may release particulate matter and system upsets, which should occur very infrequently, may cause the release of unburned hydrocarbons for a short period of time. Such upsets may occur if the incinerator is operated below the normal temperature or when the waste stream flow rate suddenly increases or the air or oxygen supply suddenly decreases. Measures to rapidly correct these situations or shut down the incinerator are provided for any well designed and operated incinerator. Public groups, however, sometimes question the effectiveness of even the best incinerators in always avoiding the release of toxic materials. The adverse effects of all potential combinations of equipment failure, system upsets, and human error are difficult to completely discount.

By means of several inherent protective mechanisms, the delayed release process of this invention greatly reduces the releases of unburned hydrocarbons or other toxic materials under both normal and upset conditions. First, only a fraction of the gas discharged from the condenser (FIG. 4) is directed to the CO<sub>2</sub> absorber, which is the only route for escape of material from the gas entering the CO<sub>2</sub> absorber; hydrocarbons, which have low solubility in aqueous solutions, would mostly remain in the gas phase and a

scrubbing tower is ineffective in removing particulate matter. Third, particulate matter, which is either transferred to the absorbent or which is formed as an insoluble species such as lead carbonate, are removed by filtering and a clear solution is delivered to the purification step of FIG. 5. Fourth, organic material is stripped out of the absorbent solution by means of a partial gas release achieved by lowering the pressure or by steam stripping.

Not only does the delayed release process provide many additional mechanisms for removal of toxic material, but it also provides a mechanism for monitoring the absorbent from which both CO<sub>2</sub> and water are released to the stack prior to the release and a means of recycling and purifying materials that do not meet specifications. It should also be noted that the use of CO<sub>2</sub> as the main carrier gas entering the incinerator rather than nitrogen, greatly reduces formation of nitrogen oxides. That which does form is effectively removed and retained by the absorbent solutions.

Two main types of absorbents may be considered for the proposed delayed release process: alkanolamines typified by monoethanolamine (MEA) and alkaline salt solutions typified by sodium carbonate. The CO<sub>2</sub> absorption is more efficient in MEA than in the carbonate salt solutions because of higher transfer rates and higher solubilities for CO<sub>2</sub>. For this reason, the MEA-type absorbents are the most commonly used. A problem with MEA is degradation, which is enhanced by oxygen in the gas from which the CO<sub>2</sub> is absorbed, and corrosion of the equipment. These problems can be mitigated by the addition of proprietary inhibitors.

The high concentration of CO<sub>2</sub> in the sidestream gas fed to the absorber mitigates the disadvantages of the alkaline salt solution processes. This is illustrated in FIG. 8 which shows a plot of the outlet CO<sub>2</sub> concentration as a function of recovery efficiency for two different inlet CO<sub>2</sub> concentrations. For an inlet CO<sub>2</sub> concentration of 18%, which is typical of the flue gas, the concentration of CO<sub>2</sub> at the outlet of the absorption tower becomes very low even at moderate recovery efficiencies. For the high CO<sub>2</sub> concentration of 75%, which would be typical of that which could be achieved in the flowsheet of FIG. 4, the CO<sub>2</sub> concentration at the outlet remains high even for up to 90% recovery efficiency. As a result, the use of alkaline salt solutions should be considered as absorbents in the proposed delayed release process, although they may be rejected in many other applications.

An advantage of the use of an inorganic absorbent is that unburned hydrocarbons can be detected by continuous

monitoring of gases driven off the solution in a small sidestream. The MEA solution might be analyzed by a similar technique, but the monitor must be capable of distinguishing between unburned hydrocarbons and MEA or its degradation products.

Various approaches in the use of alkaline salt solutions may be considered. These include the hot potassium carbonate Benfield process, which operates at an elevated pressure during absorption and releases CO<sub>2</sub> and water by reducing the pressure to cause flashing. Whereas the main recirculating gas stream to the incinerator must be maintained at slightly below atmospheric pressure, it may be possible to use elevated pressure in the side loop, which operates at low temperatures and could be tightly sealed.

While there has been disclosed what is considered to be the preferred embodiment of the present invention, it is understood that various changes in the details may be made without departing from the spirit, or sacrificing any of the advantages of the present invention.

The embodiments of the invention in which an exclusive property or privilege is claimed are defined as follows:

We claim:

1. A process for treating organic waste materials without venting gaseous emissions to the atmosphere, comprising oxidizing the organic waste materials at an elevated temperature not less than about 500° C. with a gas having an oxygen content in the range of from about 20% to about 70% to produce an oxidation product containing CO<sub>2</sub> gas, filtering the oxidation product containing CO<sub>2</sub> gas to remove particulates, contacting the particulate-free oxidation product containing CO<sub>2</sub> with an aqueous absorbent solution of alkali metal carbonates or alkanolamines to absorb a portion

of the CO<sub>2</sub> gas from the particulate-free oxidation product, and separating the CO<sub>2</sub> absorbent for further processing and recycling the remaining CO<sub>2</sub> gas for oxidation.

2. The process of claim 1, wherein the concentration of alkali metal carbonates in the aqueous solution is in the range of from about 15% by weight to about 30% by weight.

3. The process of claim 1, wherein the aqueous solution is at a temperature in the range of from about 50° C. to about 130° C. when contacted with the CO<sub>2</sub> containing gas.

4. The process of claim 1, wherein the alkali metal carbonate is present in aqueous solution at a concentration of about 20% by weight and the solution temperature is maintained in the range of from about 50° C. to about 80° C.

5. The process of claim 4, wherein the CO<sub>2</sub> absorption is conducted at about 70 psi.

6. The process of claim 1, wherein the alkali metal carbonate is potassium carbonate, sodium carbonate or mixtures thereof.

7. The process of claim 1, wherein the alkanolamine is monomethanolamine, monoethanolamine or mixtures thereof.

8. The process of claim 1, wherein about 10% to about 70% by volume of the oxidation product containing CO<sub>2</sub> is contacted with the aqueous absorbent solution, the remainder being recycled for oxidation.

9. The process of claim 8, wherein about 2 to about 20% of the CO<sub>2</sub> and water vapor absorbed in the aqueous absorbent solution is driven off and recycled to the oxidizer as a means of stripping unburned hydrocarbons from the absorbent.

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